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Electron Energy Deposition in Atomic Oxygen

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TABLE OF CONTENTS

1.	Introduction1
2.	The Secondary Electron Distribution
2.1	The Source Term S(E,t)4
2.2	Electron Impact Excitation Cross Section5
2.3	Energy Loss to Plasma Electrons7
3.0	Results7
3.1	The Loss Function for Electrons with E > 10^6 eV7
3.2	The Loss Function for Electrons with E $< 10^6$ eV8
4.0	Compa. ison and Discussion 9
5.	References11

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ELECTRON ENERGY DEPOSITION IN ATOMIC OXYGEN

1. Introduction:

High energy electrons interacting with gaseous elements produce secondary electrons which in turn generate additional ionization. A simple description of the cumulative ionization in the gas, can be made if one knows \mathbf{w}_i the energy expended by the electron in generating an ion pair. For example, in air, the energy expended to generate an ion pair is ~ 34 eV. In order to obtain \mathbf{w}_i theoretically one must perform a detailed electron energy deposition in the gas. Such a deposition, in principle, provides an abundant amount of information. It will provide the secondary electron distribution, its flux, primary and secondary electron excitation rates for the internal modes of the atom or molecule (electronic, vibrational, etc.), \mathbf{w}_i , and hence the total ionization rate. Accordingly electron energy deposition models in gaseous elements are essential and very useful in various applications; electron beam propagation in the atmosphere, electron beam generated lasers, electron beam generated discharges and their diagnostics, precipitation of energetic electrons in the upper atmosphere and auroral emissions.

There are many approaches to the electron energy deposition which may be classified 1 as follows:

- 1) Transport versus local description,
- 2) Continuous slowing down approximation versus discrete energy deposition, and
- 3) Transport or local energy loss versus Monte Carlo approach.

 An extensive literature on this subject exists, however, we allude briefly to

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some of them. For example, Green^{2,3,4} and his colleagues have used the continuous slowing down approximation to calculate electron energy deposition in atmospheric and other gaseous elements. This method has been improved^{1,5-10} by including discrete energy deposition for electrons with energy below 500 eV. Monte Carlo¹¹ and Fokker-Planck¹² methods have been utilized for energy deposition and the determination of the spatial distribution of the primary electrons. Boltzmann¹³⁻¹⁵ equation solutions have also been utilized to obtain the equilibrium distribution of the secondary electrons.

In this paper we present a model for the energy deposition in the atomic oxygen, obtain the secondary electron distribution, the efficiency of excitation to various electronic states and ionization continua and the mean energy expended for ion pair production. This effort requires, at the outset, a set of electron impact excitation and ionization cross sections for atomic oxygen. These cross sections are essential for electron energy deposition schemes and are presented in detail.

Electron deposition claculations in atomic oxygen have been performed by Dalgarno and Lejeune for the photoelectrons in the ionosphere. These photoelectrons are produced through the absorption of the solar radiation by oxygen and generally are low energy electrons ~ 100 eV. Accordingly a discrete energy deposition scheme is utilized. In their treatment electron energy dissipation to the plasma (thermal) electrons is also included. Ganas and Green have calculated loss function, L(E), in oxygen for electrons with energy E < 5 KeV. However, energy loss to plasma electrons is not considered and the range of the primary electrons (\$ 10 KeV) is higher than those considered by Dalagaro and Lejeune. Singhal and Green have considered the spatial aspects of electron energy degradation using Monte Carlo approaches for electron energies below 10 KeV. Our interest, however, is in the

interaction of high energy and high current electron beams with oxygen (E > 10 KeV). Accordingly, we utilize a new code for energy deposition in gaseous species. This code is similar in numerics to an earlier code developed at NRL 1 and has the capability to treat the super elastic collisions and its effects on the plasma electron velocity distribution, in a manner similar to that of Ref. 18.

2. The Secondary Electron Distribution:

The secondary electron distribution can be calculated 1 from Eq. 1

$$\frac{\partial N_{e}(E,t)}{\partial t} = S(E,t) - N\Sigma \sigma_{k}(E) V(E) N_{e}(E,t)$$

$$+ N\Sigma \int \sigma_{k}(E,E) V(E) N_{e}(E,t) dE$$

$$+ N_{p}(t) \frac{\partial}{\partial E} [L_{p}(E)V(E) N_{e}(E,t)]$$
(1)

where $N_e(E,t)$ is the secondary electron density per unit volume per unit energy $(cm^{-3}eV^{-1})$ and S(E,t) the production rate $(cm^{-3}sec^{-1}eV^{-1})$ due to primary electrons. The second term in the right hand side of Eq. 1 indicates the loss of the secondary electrons with energy E due to inelastic collisions resulting in excitations where the cross section for the kth excitation is denoted by $\sigma_k(E)$, V(E) the electron velocity and N the density of the atomic oxygen. The third term in Eq. (1) represents the production of a secondary electron of energy E by a higher energy electron of energy E'. The differential ionization cross section for this process is $\sigma_k(E',E)$ with the index k denoting the kth ionization continuum of oxygen. The energy loss to plasma electrons, N_p , is given by the last term on the right hand side of Eq. 1., where $L_p(E)$ is the loss function of a secondary electron with energy E to the plasma electrons. We select the bulk of the plasma electrons to be those with energy between 0.04-1.96 eV, where 1.96 eV denotes the threshold of the

excitation of the lowest oxygen electronic state (¹D). The various terms appearing in Eq. 1 are discussed in detail below.

2.1. The Source Term S(E,t)

The emphasis in this paper is on high energy electron beam deposition in oxygen. Therefore, the source term for the generation of the secondary electrons is

$$S(E,t) = j_b(E_b)\sigma_b(E_b,E) N$$
 (2)

where $j_b(E_b)$ is the number density of the beam electrons whose energy is E_b and $\sigma_b(E_b,E)$ is the differential ionization cross section. The differential ionization cross section has been measured for many molecules and atoms by Opal et al, ¹⁹ for primary electrons with energy of 2000 eV and lower. However, no measurement for atomic oxygen is available. On the other hand, Opal et al¹⁹ have observed that most of their data for the differential ionization cross section can be expressed as

$$\sigma(E_p, E_s) = C(E_p) \left[1 + (E_s/\epsilon)^2\right]^{-1}$$
(3)

where \mathbf{E}_{p} is the energy of the primary electron, $\mathbf{C}(\mathbf{E}_{p})$ a constant obtained by Eq. (4).

$$\sigma_{i}(E_{p}) = \int_{0}^{\frac{E_{p}-I}{2}} \sigma(E_{p}, E_{s}) dE_{s}$$
(4)

and ε is an average energy characteristic of each species. $\sigma_i(E_p)$ denotes the total ionization cross section for electrons with energy E_p and I the ionization energy of the atom. Therefore, one may use Eq. (3) and (4) with an

assumed value for ε and the most recent measured 20 values of the total ionization cross section and obtain $C(\Xi_p)$. The total cross section measurements in general are for electron energies up to 1000 eV. Strickland, et al 13 have used the following expression for the differential ionization cross section for oxygen.

$$\sigma(E_p, E_s) = \frac{2}{E_p - I} \sigma_I(E_p) \text{ for } E_p < I + 10$$
 (5a)

$$\sigma(E_p, E_s) = C(E_p) \left\{ \frac{1}{\epsilon^2 + 25} + \frac{1}{\epsilon^2 + (E_p - I - 5)^2} \right\}$$

$$-\frac{1}{\varepsilon^{2} + 5(E_{p}-I_{-5})}, \text{ for } E_{b} \ge I+10$$

$$E_{q} \le 5$$
(5b)

$$\sigma(E_{p}, E_{s}) = C(E_{p}) \cdot \left\{ \frac{1}{E_{s}^{2} + \epsilon^{2}} + \frac{1}{\epsilon^{2} + (E_{p} - I - E_{s})^{2}} \right\}$$

$$= \frac{1}{E_{s}^{2} + \epsilon^{2}} \cdot \left\{ \frac{1}{E_{p}^{2} + (E_{p} - I - E_{s})^{2}} + \frac{1}{E_{s}^{2} + (E_{p} - I - E_{s})^{2}} \right\}$$
(5e)

$$-\frac{1}{\varepsilon^2 + E_s(E_p - I - E_s)} \}, \text{ for } E_p \ge I + 10$$

$$E_s > 5$$

However, for relativistic electrons one must use Moellers' formula. 21

To obtain the fractional ionization leading to various ionization continuum i.e., $0^+(^4S)$, $0^+(^2D)$ and $0^+(^2P)$ we use the fractions obtained by Dalgarro and Lejeune⁹. Using these fractions we give the total and the fractional ionization cross sections as a function of the electron energy, (see Table 1).

2.2 Electron Impact Excitation Cross Section

In discussing the electron impact excitations of oxygen electronic states, one may divide the excitations into several categories. First, the low lying metastable states of oxygen $O(^{1}D)$ and $O(^{1}S)$ which belong to the

ground state configuration of the atom. These cross sections have been calculated by numerous workers (for details see Ref. 22) and those by Thomas and Nisbet, ²³ which are preferred, ²² are shown in Fig. 1 and are given in Table II. The second group of electronic states are those with dipole allowed transitions to the ground state. For these states, the following expression given by Drawin, ²⁴ can be used.

$$\sigma_{ij} = 3.5 \times 10^{-16} f_{ij} \left(\frac{13.6}{E_{ij}}\right)^2 \left(\frac{E_{ij}}{E}\right)^2 \left(\frac{E}{E_{ij}} - 1\right) \log \left(1.25 - \frac{E}{E_{ij}}\right)$$
 (6)

Here, f_{ij} is the oscillator strength for the transition from state i to j whose excitation energy is E_{ij} . Using Eq. 6 the electron impact excitation for the transition $^3p \rightarrow ^3s$ (the resonance line) is shown in Figure 2. The experimental data for the absolute cross section 25,26 is also shown in Fig. 2 along with other theoretical $^{27-29}$ calculations. It is obvious that the experimental data is higher than the theortical calculations because the experimental data includes cascade from higher states. However, we normalize our calculations to 0.5 of the experimental value making our result in good accord with Ref. 27. The appropriate parameters for the optically allowed transitions are given in Table III.

For forbidden transitions e.g. $^3p-^5s^0$ we utilize the experimental data 26 (see Table IV). For higher states we use the parametric fits developed by Jackman et al 30 where the cross section is expressed as

$$\sigma_{ij} = \frac{6.5 \times 10^{-14} \text{Cf}_{ij}}{E_{ij}^2} \left(1 - \frac{E_{ij}}{E}\right)^{\nu} \left(\frac{E_{ij}}{E}\right)^{\Omega}$$
 (7)

and the appropriate parameters are given in Table V.

As for higher Rydberg states, we obtain the asymptotic values of the oscillator strength using he quantum defect method. For these and other states included in the expression, see Table V and Fig. 3.

2.3. Energy Loss to Plasma Electrons:

Perkins³¹ has derived the rate of energy loss to plasma electrons by a test electron. These results have been utilized by Schunk and Hays³² to obtain the following expressions for the energy loss

$$\frac{dE}{dt} = \frac{\omega_p^2 e^2}{v^2} \log \frac{mv^3}{\gamma e^2 \omega_p} \qquad \text{for } kT \ll E \ll \frac{me^4}{2k^2}$$
 (8)

$$= \frac{\omega_p^2 e^2}{v^2} \log \frac{mv^2}{h\omega_p} \qquad \text{for } E > \frac{me^4}{26^2}$$
 (9)

where ω_p is the plasma frequency. These can be expressed, in terms of the loss function (see Eq. 1), as

$$L_p(E) = \frac{1.3 \times 10^{-13}}{E} \log \frac{8.2 \times 10^9 E^{1.5}}{\sqrt{N_p}}, E < 20 \text{ eV}$$
 (10)

$$L_p(E) = \frac{1.3 \times 10^{-13}}{E} \log \frac{5.4 \times 10^{10}}{\sqrt{N_p}} E$$
, $E > 20 \text{ eV}$ (11)

3.0. Results:

3.1. The Loss Function For Electrons with $E > 10^6$ eV.

For electrons with energy above $E = 10^6$ we utilize the Bethe-Bloch³³ equation to calculate the stopping power. The relativistic form of the loss function³³ is

$$L(E) = \frac{2\pi r_0^2 \text{mc}^2}{\beta^2} Z \left[\log \frac{T^2}{I^2} \frac{(\gamma+1)}{2} + 1 - \beta^2 - \frac{2\gamma-1}{\gamma^2} \log 2 + \frac{1}{8} \left(\frac{\gamma-1}{\gamma}\right)^2 \right]$$
(12)

Where r_0 is the classical electron radius, Z the atomic number, T the kinetic energy of the electron and E the total energy and I the mean excitation energy which is equal to 89 eV for oxygen. We have used Eq. (12) to calculate the loss function in oxygen for T = 100 MeV down to T = 10^4 eV and show the result in Figure 3. It should be noted that our results are in good agreement with the calculations of Pages et al. 34 However, using Eq. 12 to obtain the loss function one obtains only the information on the energy loss per unit path. One does not obtain any other information e.g. the secondary electron distribution, its flux, the efficiency of excitation of individual excitation channels, and the energy per ion pair. Accordingly, our discrete deposition scheme does provide this relevant information.

3.2. The Loss Function for Electrons With E $< 10^6$ eV

The discrete energy deposition scheme described in detail in this report is utilized for primary electrons with E $< 10^6$ eV and the results are discussed in this Section. The loss function can be written as in Eq. (13).

 $\sum_{j} W_{j} \sigma_{j}(E) + \sum_{j} I_{j} \sigma_{I}(E) + \sum_{j} \sum_{s} I_{j} \sigma_{I}(E, E_{s}) dE_{s}$ (13)

where the first term is a sum over excited states with excitation energy W_j and cross section $\sigma_j(E)$; the second term is a sum over ionization states with ionization energy I_j and cross section $\sigma_{Ij}(E,E_s)$ and the third term sums the amount of energy going into the secondaries with $E_{sjmax} = (E-I_j)/2$ the maximum secondary energy and $\sigma_{Ij}(E,E_s)$ the differential ionization cross section for the jth ionization state. Using Eq. (13) we obtain L(E) and show the results for electron enegies of 500 to 10^6 eV. The serious are shown in Table VI. The percentages of the loss function going into these three channels is described in Eq. (13) are also given in Table VI. Figure 4 shows a plot of L(E) and its three terms.

The third row of Table VI gives W_i the energy expended to create an ion pair. For a given beam and oxygen background the number of ion pairs created per cubic cm per second is $\frac{1}{W_i}$ $\frac{dE}{dX}$ F where F is the beam flux in beam particles per cm² per sec. W_i is fairly constant throughout this energy range but increases dramatically for lower beam energies because the ratio of the excitation cross section to the ionization cross section gets larger. The fourth and fifth lines of Table VI give the percentage of ion pairs created directly from ionization by a beam electron - called first generation secondaries - and those created in the ensuing cascade.

Figure 5 shows the steady state secondary electron distribution function N_e while Figure 6 shows the flux ϕ = Ne V . In all cases the beam flux was $F = 1.99 \times 10^{18}$ electrons per cm² per sec and the background was 2.46 x 10^{19} atoms of oxygen per cm³.

Finally Table VII gives the production efficiencies for all the states in the model. The production efficiency of a state is defined to be the number of excitations of that state per ion pair created. Therefore the creation rate for a state is given by $P = \frac{1}{W_{\hat{I}}} = \frac{dE}{dX}$ F where P is the appropriate production efficiency.

4.0. Comparison and Discussion:

The loss function, L(E), calculated by the discrete method, shown in Fig. 4, is replotted in Fig. 7, for comparison with the results predicted by Bethe's non relativistic expression and the calculations of Ganas and Green¹⁶. The discrete calculation is lower than what is predicted by Bethe's equation. The disagreement is $\sim 12\%$ at E = 10^4 and 25% at the E = 10^3 eV. However, the results of Ref. 16 are higher than those predicted by Bethe's equation and our own calculation.

The energy per ion pair predicted by our code is - 28 eV over a wide electron energy range (500-100,000 eV). There is no data, as far as we know,

method for the total absorption of the photoelectrons (E < 100 eV) in the ionosphere. They predict a value of 29 eV per electron ion pair. To compare our results with those of Lalgarno and Lejeune we ran our code for incident electrons of 100 and 50 eV for the case of a completely stopped electron, as done by Dalgarno and Lejeune. Our results for the energy per ion pair are 33.6 eV and 40.4 eV, respectively compared to 29 and 34, read from Fig. 13 of Ref. 9, for the case of a very low ionization fraction present in the gas. These results are fairly comparable.

In comparing our results with those of Ganas and Green 16 we note that they utilize the concept of generalized oscillator strength in obtaining excitation and ionization cross sections. One reason for their L(E) being larger than ours can be traced to their higher expression for the ionization cross section compared to the experimental data, which we use. For example at $E = 10^2$ eV they predict an ionization cross section of 3×10^{-16} cm² compared to the experimental data²⁰ of 1.3×10^{-16} cm². Their ionization cross sections however, fits the experimental data much better at E = 5000 eV. Here, their results for L(E) is higher than ours by 15% while their L(E) at E = 100 eV is nearly twice of ours and also much higher than that predicted by Bethe's equation.

Dalgarno and Lejeune do not report the calculations of L(E), however, they do calculate certain excitation efficiencies of excited states, specifically those of $O(^1D)$. In comparing our calculations with those of Ref. 9 we find an excitation efficiency for $O(^1D)$ at E = 100 eV to be twice as large as theirs. This certainly is due to the fact that they use the calculated cross sections of Henry, et al³⁵, while we utilize the more recent calculations of Thomas and Nisbet²³ which we believe to be more accurate. We can not compare excitation efficiencies with Ganas and Green, because in the

first place they do not consider the forbidden states of oxygen ¹D, and ¹S, etc. Furthermore, in their evaluation of the contribution of energy deposited to excitation and ionization they indicate that most of the energy goes into ionization. Our result does not show such a phenomena. Indeed, in our calculations we see that considerable energy is stored in the ¹D state. This discrepancy may be due to the fact that Ganas and Green have ignored those, and other forbidden states of oxygen.

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Table I - Ionization Cross Section of 0

<u>E</u>	<u>σ</u>	a(13.6)	b(16.93)	c(18.62)
13.6	0 -			
17	2.1(-17)	2.1(-17)	•	
20.4	3:37(-17)	2:2(-17)	0.95(-17)	0.18(-17)
23:8	4.64(-17)	3:04(-17)	1:3(-17)	0:26(-17)
27:2	5.89(-17)	3:03(-17)	2:0(-17)	0:85(-17)
30:6	7:05(-17)	3:27(-17)	2:54(-17)	1:23(-17)
34	8:1(-17)	3.76(-17)	2:92(-17)	1.42(-17)
37.4	9:0(-17)	3:91(-17)	3:39(-17)	1:69(-17)
40.8	9:8(-17)	4:07(-17)	3:86(-17)	1.86(-17)
47.6	1:1(-16)	3.91(-17)	4:15(-17)	2:06(-17)
54.4	1:19(-16)	4:52(-17)	4:76(-17)	2:52(-17)
61:2	1.25(-16)	4:74(-17)	5:0(-17)	2:6(-17)
68	1.29(-16)	4.77(-17)	5.28(+17)	2:7(-17)
81.6	1:34(-16)	4.95(-17)	5:5(-17)	2:8(-17)
95:2	1:35(-16)	4.95(-17)	5:5(-17)	2.8(-17)
108:8	1:34(-16)	0.37 or	0:41 a _T	0:21 o _T
122:4	1:33(-16)			
136.2	1:30(-16)			
170	1:24(-16)			
204	1:17(-16)			
272	1:04(-16)			
408	8.57(-17)			
544	7:32(-17)			
680	6:4(-17)			
1020	4:9(-17)			
1360	4:1(-17)			

For
$$10^3 < E < 10^5$$
 use $\sigma_T = \frac{1.8 \times 10^{-14}}{E} \log (E/13.6)$

Table II — Electron Impact Excitation Cross Section of 0(1D) and 0(1S)

Energy(eV)	O(1D)	σ (10 ⁻¹⁷ cm	1 ²)
2.0		0	
3.0		0.97	
4:0		1.85	
5:0		2:4	
6.0		2:58	
7:0		2.52	
8:0		2.40	
9:0		2:25	
10:0		1.97	

11.0 and higher E use $\sigma = 2.62 \times 10^{-14} / E^3$

Energy(eV)	0(15)		$\sigma (10^{-18} \text{cm}^2)$
4		0.98	
5		1.3	
5 6		1.8	
		1:97	
7 8		2:0	
9		2:37	
10		2.6	
			15 2
11 and high	er E use a =	3.46x10	15 _{/E} 3

Table III - States with Optically Allowed Transitions to the Ground State

State	Excitation Energy (eV)	Oscillator Strength
3s ³ S°	9.5	0.046
3d 3D.	12.10	0.01
3s, 3D°	12.50	0.056
3s, 3po	14.10	0.037
3d, 3po	15.3	0.0077
		•

Table IV — Electron Impact Excitation of $3_p - 5_s$

Energy	$\sigma(10^{-17}\mathrm{cm}^2)$
10	0.107
11.2	1.17
15	2.5
20	1.62
40	0.42
50	0.25
55	0.2
Higher	$\sigma = 3.1 \times 10^{-13} / E^3$

Table V - Cross Section Parameters for Rydberg and Other Forbidden States

σ	E _{ij}	С	f _{ij}	ν	Ω
σ _{R1}	11.93	0.018	1.5	2.5	0.7
σ _{R2}	12.76	0.008	1.5	2.5	0.7
σ _{R3}	16.11	0.0065	1.5	2.5	0.7
σ _{R4}	11.0	0.053	0.07	0.5	0.7
σ _{R5}	14.5	0.065	0.07	0.5	0.7
σ _{R6}	15.8	0.043	0.07	0.5	0.7
σ _R 7	14.1	0.055	0.1	1.0	1.0
σ _{R8}	10.7	0.068	0.3	1.0	2.0
σ _{R9}	14.0	0.08	0.3	1.0	2.0
σ _{R10}	15.8	0.054	0.3	1.0	2.0
σ _{R11}	12.7	0.065	0.4	1.0	2.0
σ _{R12}	12.1	0.043	0.4	1.0	2.0
σ _{R13}	14.1	0.065	0.14	1.0	2.0

Table VI - Summary of Results

Incident Energy	500 eV	1 KeV	5ке v	10 KeV	50 KeV	100 KeV	500 KeV	1 MeV
Loss Function L(E) (eV-cm ²)	2,78(-15)	1.92(-15)	6.83(-16)	6.83(-16) 4.12(-16)	1.20(-16)	1.20(-16) 6.92(-17)	1.86(-17)	1.04(-17
Energy per ion pair $W_{\underline{\mathbf{I}}}$ (eV)	7.72	27.1	27.7	27.8	27.8	27.8	27.9	28.0
<pre>\$ of ion pairs due to 1st generation secondaries</pre>	75	69	57	53	911	f ₁ 3	38	36
% of ion pairs due to the rest of secondaries	25	31	43	<i>μ</i> 7	54	57	62	ħ9
% of beam deposition in excitation	ω	, c	9	2	2	코	ੜ	म
% of beam deposition in ionization	ħħ	1	33	31	26	25	22	23
% of beam deposition in 1st generation secondary energy	811	54	61	ф9	69	11	7.4	75

(Rows 4-6 are the 3 forbidden states. Rows 7-11 are the optically allowed states in the order given in Table III.)

0+42	D P 1-3F 1-4F 1-5 1-6 1-7 1-8 R 2 R R R R R R R R R R R R R R R R R	Dir 0.281 0.311 0.160 0.000 0.000 0.000 0.103 0.008 0.042 0.024 0.005 0.003 0.003 0.003 0.003 0.001 0.001 0.001 0.000 0.000 0.000	Sec 0.119 0.088 0.042 2.017 0.062 0.125 0.198 0.003 0.004 0.003 0.005 0.002 0.001 0.005 0.002 0.001 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005	Total 0.400 0.399 0.202 2.017 0.082 0.125 0.300 0.018 0.042 0.008 0.014 0.005 0.003 0.003 0.002 0.002 0.002 0.003 0.003 0.003 0.003 0.003 0.004
0	R13	0.000 1 Ke	0.001	0.001
Spe	cies	Dir	Sec	Total
0+4		0.258	0.142	0.400
0+2		0.286	0.113	0.399
0	1-2F	0.000	2.018	2.018
0	1-3F	0.000	0.063	0.063
0	1-4F	0.000	0.126	0.126
0	1-4F 1-4	0.000	0.126	0.126
0	1-4F	0.000	0.126	0.126
00000	1-4F 1-4 1-5 1-6 1-7	0.000 0.060 0.005 0.025 0.014	0.128 0.211 0.009 0.048 0.021	0.126 0.272 0.014 0.072 0.035
000000	1-4F 1-4 1-5 1-6 1-7 1-8	0.000 0.060 0.005 0.025 0.014 0.003	0.126 0.211 0.009 0.046 0.021 0.003	0.126 0.272 0.014 0.072 0.035 0.006
000000	1-4F 1-4 1-5 1-6 1-7 1-8 R 1	0.000 0.060 0.005 0.025 0.014 0.003 0.006	0.126 0.211 0.009 0.046 0.021 0.003 0.007	0.126 0.272 0.014 0.072 0.035 0.006 0.012
00000000	1-4F 1-4 1-5 1-6 1-7 1-8	0.000 0.060 0.005 0.025 0.014 0.003 0.006 0.002	0.126 0.211 0.009 0.046 0.021 0.003 0.007 0.002	0.126 0.272 0.014 0.072 0.035 0.006 0.012 0.005
000000000	1-4F 1-4 1-5 1-6 1-7 1-8 R 1 R 2 R 3 R 4	0.000 0.060 0.005 0.025 0.014 0.003 0.006 0.002 0.001	0.126 0.211 0.009 0.046 0.021 0.003 0.007 0.002 0.001	0.126 0.272 0.014 0.072 0.035 0.006 0.012 0.005 0.002
00000000000	1-4F 1-4 1-5 1-6 1-7 1-8 R 1 R 2 R 3 R 4 R 5	0.000 0.060 0.005 0.025 0.014 0.003 0.006 0.002 0.001 0.001	0.126 0.211 0.009 0.046 0.021 0.003 0.007 0.002 0.001 0.005 0.002	0.126 0.272 0.014 0.072 0.035 0.006 0.012 0.005 0.002 0.006
000000000000	1-4F 1-4 1-5 1-6 1-7 1-8 R 1 R 2 R 3 R 4 R 5 R 6	0.000 0.080 0.005 0.025 0.014 0.003 0.006 0.002 0.001 0.001	0.126 0.211 0.009 0.046 0.021 0.003 0.007 0.002 0.001 0.005 0.002	0.126 0.272 0.014 0.072 0.035 0.006 0.012 0.005 0.002 0.003 0.003
0000000000000	1-4F 1-5 1-6 1-7 1-8 R 1 R 2 R 3 R 4 R 5 R 6	0.000 0.060 0.005 0.025 0.014 0.003 0.006 0.002 0.001 0.001 0.001 0.000	0.126 0.211 0.009 0.046 0.021 0.003 0.007 0.002 0.001 0.005 0.002	0.126 0.272 0.014 0.072 0.035 0.006 0.012 0.005 0.002 0.003 0.002
000000000000	1-4F 1-4 1-5 1-6 1-7 1-8 R 1 R 2 R 3 R 4 R 5 R 6	0.000 0.080 0.005 0.025 0.014 0.003 0.006 0.002 0.001 0.001	0.126 0.211 0.009 0.046 0.021 0.003 0.007 0.002 0.001 0.005 0.002	0.126 0.272 0.014 0.072 0.035 0.006 0.012 0.005 0.002 0.003 0.003
0000000000000000	1-4F 1-4 1-5 1-6 1-7 1-8 R 1 R 2 R 3 R 4 R 5 R 6 R 7 R 8	0.000 0.060 0.005 0.025 0.014 0.003 0.006 0.002 0.001 0.001 0.001 0.000 0.000 0.000	0.126 0.211 0.009 0.046 0.021 0.003 0.007 0.002 0.001 0.005 0.002 0.001 0.001 0.009 0.004 0.002	0.126 0.272 0.014 0.072 0.035 0.006 0.012 0.005 0.002 0.003 0.002 0.002 0.002
00000000000000000	1-4F 1-4 1-5 1-6 1-7 1-8 R 1 R 2 R 3 R 4 R 6 R 7 R 8 R 9 R10	0.000 0.060 0.005 0.025 0.014 0.003 0.006 0.002 0.001 0.001 0.001 0.000 0.000 0.000 0.000	0.126 0.211 0.009 0.046 0.021 0.003 0.007 0.002 0.001 0.005 0.002 0.001 0.001 0.009 0.004 0.002	0.126 0.272 0.014 0.072 0.035 0.006 0.012 0.005 0.002 0.003 0.002 0.002 0.002 0.004 0.002
0000000000000000	1-4F 1-4 1-5 1-6 1-7 1-8 R 1 R 2 R 3 R 4 R 5 R 6 R 7 R 8	0.000 0.060 0.005 0.025 0.014 0.003 0.006 0.002 0.001 0.001 0.001 0.000 0.000 0.000	0.126 0.211 0.009 0.046 0.021 0.003 0.007 0.002 0.001 0.005 0.002 0.001 0.001 0.009 0.004 0.002	0.126 0.272 0.014 0.072 0.035 0.006 0.012 0.005 0.002 0.003 0.002 0.002 0.002

		5 Ke		
Spec		Dir	Sec	Total
0+45		0.215	0.188	0.401
0+21		0.238	0.161	0.201
0	1-2F	0.000	2.020	2.020
0	1-3F	0.000	0.083	0.063
0	1-4F	0.000	0.127	0.127
0	1-4	0.069	0.231	0.300
0	1-5	0.005	0.011	0.016
o	1-6	0.029	0.054	0.083
Ö	1-7	0.017	0.025	0.042
0	1-8	0.003	0.004	0-008
0	R 1	0.007	0.008	0.015
0	R 2	0.003	0.003	0.006
0	R 3	0.002	0.001	0.003
0	R 4	0.001	0.006	0.007
0	R 5	0.001	0.003	0.003
0	R 6	0.001	0.001	0.002
0	R 7	0.000	0.002	0.002
0	R 8	0.000	0.009	0.009
0	R 9	0.000	0.004	0.004
0	R10	0.000	0.002	0.002
0	R11	0.000	0.006	0.006
0	R12	0.000	0.004	0.004
0	R13	0.000	0.001	0.001
		10 3	(eV	
Spe	cies	Dir	Sec	Total
0+4	S	0.200	0.201	0.401
0+2		0.221	0.178	0.399
0+2		0.113	0.087	0.201
0	1-2F			
0		0.000	2.020	2.020
	1-3F	0.000	0.063	0.063
0	1-3F 1-4F	0.000	0.063	0.063
0	1-3F 1-4F 1-4	0.000 0.000 0.063	0.063 0.127 0.237	0.063 0.127 0.300
0 0	1-3F 1-4F 1-4 1-5	0.000 0.000 0.063 0.005	0.063 0.127 0.237 0.011	0.063 0.127 0.300 0.016
0 0 0	1-3F 1-4F 1-4 1-5 1-6	0.000 0.000 0.063 0.005 0.027	0.063 0.127 0.237 0.011 0.056	0.063 0.127 0.300 0.016 0.083
00000	1-3F 1-4F 1-4 1-5 1-6 1-7	0.000 0.000 0.063 0.005 0.027 0.016	0.063 0.127 0.237 0.011 0.056 0.028	0.063 0.127 0.300 0.016 0.083 0.042
00000	1-3F 1-4F 1-4 1-5 1-6 1-7	0.000 0.000 0.063 0.005 0.027 0.016 0.003	0.063 0.127 0.237 0.011 0.056 0.026 0.005	0.063 0.127 0.300 0.016 0.083 0.042 0.008
0 0 0 0 0 0	1-3F 1-4F 1-4 1-5 1-6 1-7 1-8 R 1	0.000 0.000 0.063 0.005 0.027 0.016 0.003	0.063 0.127 0.237 0.011 0.056 0.026 0.005	0.063 0.127 0.300 0.016 0.083 0.042 0.008 0.016
0000000	1-3F 1-4F 1-4 1-5 1-6 1-7 1-8 R 1 R 2	0.000 0.000 0.063 0.005 0.027 0.016 0.003 0.007	0.063 0.127 0.237 0.011 0.056 0.026 0.005 0.009	0.063 0.127 0.300 0.016 0.083 0.042 0.008
00000000	1-3F 1-4F 1-4 1-5 1-6 1-7 1-8 R 1	0.000 0.000 0.063 0.005 0.027 0.016 0.003	0.063 0.127 0.237 0.011 0.056 0.026 0.005	0.063 0.127 0.300 0.016 0.083 0.042 0.008 0.016 0.006
0000000	1-3F 1-4F 1-4 1-5 1-6 1-7 1-8 R 1 R 2 R 3	0.000 0.000 0.063 0.005 0.027 0.016 0.003 0.007 0.003	0.063 0.127 0.237 0.011 0.056 0.026 0.005 0.009 0.003	0.063 0.127 0.300 0.016 0.083 0.042 0.008 0.016 0.006 0.003 0.007
00000000000	1-3F 1-4F 1-5 1-6 1-7 1-8 R 1 R 2 R 3 R 4 R 5 R 6	0.000 0.000 0.063 0.005 0.027 0.016 0.003 0.007 0.003 0.002 0.001	0.063 0.127 0.237 0.011 0.056 0.028 0.005 0.005 0.003 0.001 0.006 0.003	0.063 0.127 0.300 0.016 0.083 0.042 0.008 0.016 0.006 0.003 0.007 0.004 0.002
000000000000	1-3F 1-4F 1-4 1-5 1-6 1-7 1-8 R 1 R 2 R 3 R 4 R 5 R 6 R 7	0.000 0.000 0.063 0.005 0.027 0.016 0.003 0.007 0.003 0.002 0.001	0.063 0.127 0.237 0.011 0.056 0.028 0.005 0.009 0.003 0.001 0.006 0.003	0.063 0.127 0.300 0.016 0.083 0.042 0.008 0.016 0.006 0.003 0.007 0.004 0.002 0.002
000000000000	1-3F 1-4F 1-4 1-5 1-6 1-7 1-8 R 1 R 2 R 3 R 4 R 5 R 6 R 7	0.000 0.000 0.063 0.005 0.027 0.016 0.003 0.007 0.003 0.002 0.001 0.001	0.063 0.127 0.237 0.011 0.056 0.026 0.005 0.009 0.003 0.001 0.006 0.003	0.063 0.127 0.300 0.016 0.083 0.042 0.008 0.016 0.005 0.003 0.007 0.004 0.002 0.002
0000000000000	1-3F 1-4F 1-4 1-5 1-6 1-7 1-8 R 1 R 2 R 3 R 4 R 5 R 6 R 7	0.000 0.000 0.063 0.005 0.027 0.016 0.003 0.007 0.003 0.002 0.001 0.001	0.063 0.127 0.237 0.011 0.056 0.026 0.005 0.009 0.003 0.001 0.006 0.003 0.001	0.063 0.127 0.300 0.016 0.083 0.042 0.008 0.016 0.003 0.007 0.004 0.002 0.002 0.009
000000000000000	1-3F 1-4F 1-4 1-5 1-6 1-7 1-8 R 1 R 2 R 3 R 4 R 5 R 6 R 7 R 8	0.000 0.000 0.063 0.005 0.027 0.016 0.003 0.007 0.003 0.002 0.001 0.001	0.063 0.127 0.237 0.011 0.056 0.026 0.005 0.009 0.003 0.001 0.006 0.003 0.001	0.063 0.127 0.300 0.016 0.083 0.042 0.008 0.016 0.003 0.007 0.004 0.002 0.002 0.009 0.004 0.002
0000000000000000	1-3F 1-4F 1-4 1-5 1-6 1-7 1-8 R 1 R 2 R 3 R 4 R 5 R 6 R 7 R 8 R 9 R10 R11	0.000 0.000 0.063 0.005 0.027 0.016 0.003 0.007 0.003 0.002 0.001 0.001 0.001	0.063 0.127 0.237 0.011 0.056 0.026 0.005 0.009 0.003 0.001 0.006 0.003 0.001 0.002 0.002 0.004 0.002 0.003	0.063 0.127 0.300 0.016 0.083 0.042 0.008 0.016 0.003 0.007 0.004 0.002 0.002 0.009 0.004 0.002 0.002
000000000000000	1-3F 1-4F 1-4 1-5 1-6 1-7 1-8 R 1 R 2 R 3 R 4 R 5 R 6 R 7 R 8	0.000 0.000 0.063 0.005 0.027 0.016 0.003 0.007 0.003 0.002 0.001 0.001	0.063 0.127 0.237 0.011 0.056 0.026 0.005 0.009 0.003 0.001 0.006 0.003 0.001	0.063 0.127 0.300 0.016 0.083 0.042 0.008 0.016 0.003 0.007 0.004 0.002 0.002 0.009 0.004 0.002

			eV_	Tentral 1
	cies	Dir	Sec	Total
0+4	5	0.171	0.230	0.400
0+21	D	0.189	0.209	0.399
0+2	P	0.097	0.104	0.201
0	1-2F	0.000	2.024	2.024
0	1-3F	0.000	0.063	0.063
0	1-4F	0.000	0.126	
				0.126
0	1-4	0.053	0.247	0.300
0	1-5 -	0.004	0.012	0.016
0	1-6	0.023	0.061	0.083
0	1-7	0.013	0.029	0.042
0 .	1-8	0.003	0.005	0.008
0	R 1	0.008	0.010	0.018
0	R 2	0.003	0.004	0.007
0	R 3	0.002	0.002	0.004
0	R 4	0.001	0.006	0.007
Ö	R 5	0.001	0.003	0.004
	R 6	0.001		0.002
0			0.001	
0	R 7	0.000	0.002	0.002
0	R 8	0.000	0.009	0.009
0	R 9	0.000	0.004	0.004
0	R10	0.000	0.002	0.002
0	R11	0.000	0.006	0.008
0	R12	0.000	0.004	0.004
0	R13	0.000	0.001	0.001
			KeV .	
	cies	Dir	Sec	Total
0+4	S	Dir 0.161	Sec 0.240	0.401
0+4	S D	Dir 0.161 0.178	Sec 0.240 0.220	0.401
0+4: 0+2: 0+2:	S D P	Dir 0.161 0.178 0.091	Sec 0.240 0.220 0.109	0.401 0.399 0.201
0+4: 0+2: 0+2:	S D P 1-2F	Dir 0.161 0.178 0.091 0.000	Sec 0.240 0.220 0.109 2.019	0.401 0.399 0.201 2.019
0+4: 0+2: 0+2: 0	S D P 1-2F 1-3F	Dir 0.161 0.178 0.091 0.000 0.000	Sec 0.240 0.220 0.109 2.019 0.063	0.401 0.399 0.201 2.019 0.063
0+4: 0+2: 0+2:	S D P 1-2F	Dir 0.161 0.178 0.091 0.000	Sec 0.240 0.220 0.109 2.019	0.401 0.399 0.201 2.019
0+4: 0+2: 0+2: 0	S D P 1-2F 1-3F	Dir 0.161 0.178 0.091 0.000 0.000	Sec 0.240 0.220 0.109 2.019 0.063	0.401 0.399 0.201 2.019 0.063
0+4: 0+2: 0+2: 0	S D P 1-2F 1-3F 1-4F	Dir 0.161 0.178 0.091 0.000 0.000	Sec 0.240 0.220 0.109 2.019 0.063 0.127	0.401 0.399 0.201 2.019 0.063 0.127
0+4: 0+2: 0 0 0 0	S D P 1-2F 1-3F 1-4F 1-4	Dir 0.161 0.178 0.091 0.000 0.000 0.000	Sec 0.240 0.220 0.109 2.019 0.063 0.127 0.251	0.401 0.399 0.201 2.019 0.063 0.127 0.301
0+4: 0+2: 0 0 0 0 0	S D P 1-2F 1-3F 1-4F 1-4 1-5	Dir 0.161 0.178 0.091 0.000 0.000 0.000 0.050 0.004	Sec 0.240 0.220 0.109 2.019 0.063 0.127 0.251 0.012 0.062	0.401 0.399 0.201 2.019 0.063 0.127 0.301 0.016 0.084
0+4: 0+2: 0+2: 0 0 0 0	S D P 1-2F 1-3F 1-4F 1-4 1-5 1-6 1-7	Dir 0.161 0.178 0.091 0.000 0.000 0.000 0.050 0.004 0.021 0.012	Sec 0.240 0.220 0.109 2.019 0.063 0.127 0.251 0.012 0.062 0.029	0.401 0.399 0.201 2.019 0.063 0.127 0.301 0.016 0.084 0.042
0+4: 0+2: 0+2: 0 0 0 0	S D D D D D D D D D D D D D D D D D D D	Dir 0.161 0.178 0.091 0.000 0.000 0.000 0.050 0.004 0.021 0.012 0.002	Sec 0.240 0.220 0.109 2.019 0.063 0.127 0.251 0.012 0.062 0.029 0.005	0.401 0.399 0.201 2.019 0.063 0.127 0.301 0.016 0.084 0.042 0.008
0+4: 0+2: 0+2: 0 0 0 0 0 0	S D D D D D D D D D D D D D D D D D D D	Dir 0.161 0.178 0.091 0.000 0.000 0.050 0.050 0.004 0.021 0.012 0.002 0.009	Sec 0.240 0.220 0.109 2.019 0.063 0.127 0.251 0.012 0.062 0.029 0.005 0.010	0.401 0.399 0.201 2.019 0.063 0.127 0.301 0.016 0.084 0.042 0.008 0.019
0+4: 0+2: 0+2: 0 0 0 0 0 0	S D D D D D D D D D D D D D D D D D D D	Dir 0.161 0.178 0.091 0.000 0.000 0.050 0.004 0.021 0.012 0.002 0.009	Sec 0.240 0.220 0.109 2.019 0.063 0.127 0.251 0.012 0.062 0.029 0.005 0.010 0.004	0.401 0.399 0.201 2.019 0.063 0.127 0.301 0.016 0.084 0.042 0.008 0.019 0.007
0+4: 0+2: 0+2: 0 0 0 0 0 0 0 0	S D D D D D D D D D D D D D D D D D D D	Dir 0.161 0.178 0.091 0.000 0.000 0.050 0.004 0.021 0.012 0.002 0.009 0.004	Sec 0.240 0.220 0.109 2.019 0.063 0.127 0.251 0.012 0.062 0.029 0.005 0.010 0.004 0.002	0.401 0.399 0.201 2.019 0.063 0.127 0.301 0.016 0.084 0.042 0.008 0.019 0.007
0+4: 0+2: 0+2: 0 0 0 0 0 0 0 0	S D D D D D D D D D D D D D D D D D D D	Dir 0.161 0.178 0.091 0.000 0.000 0.050 0.004 0.021 0.012 0.002 0.009 0.004 0.002	Sec 0.240 0.220 0.109 2.019 0.063 0.127 0.251 0.012 0.062 0.029 0.005 0.010 0.004 0.002 0.006	0.401 0.399 0.201 2.019 0.063 0.127 0.301 0.016 0.084 0.042 0.008 0.019 0.007
0+4: 0+2: 0+2: 0 0 0 0 0 0 0 0 0 0	S D D D D D D D D D D D D D D D D D D D	Dir 0.161 0.178 0.091 0.000 0.000 0.050 0.004 0.021 0.012 0.002 0.009 0.004 0.002	Sec 0.240 0.220 0.109 2.019 0.063 0.127 0.251 0.012 0.062 0.029 0.005 0.010 0.004 0.002 0.006 0.003	0.401 0.399 0.201 2.019 0.063 0.127 0.301 0.016 0.084 0.042 0.008 0.019 0.007 0.004
0+4: 0+2: 0+2: 0 0 0 0 0 0 0 0 0 0 0 0 0	S D P 1-2F 1-3F 1-4F 1-5 1-6 1-7 1-8 R 1 R 2 R 3 R 6	Dir 0.161 0.178 0.091 0.000 0.000 0.050 0.050 0.021 0.012 0.002 0.009 0.009 0.004 0.002	Sec 0.240 0.220 0.109 2.019 0.063 0.127 0.251 0.012 0.062 0.029 0.005 0.010 0.004 0.002 0.006 0.003 0.001	0.401 0.399 0.201 2.019 0.063 0.127 0.301 0.016 0.084 0.042 0.008 0.019 0.007 0.004 0.007
0+4: 0+2: 0+2: 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	S D P 1-2F 1-3F 1-4F 1-5 1-6 1-7 1-8 R 2 R 5 R 7	Dir 0.161 0.178 0.091 0.000 0.000 0.000 0.050 0.004 0.021 0.012 0.002 0.009 0.004 0.002	Sec 0.240 0.220 0.109 2.019 0.063 0.127 0.251 0.012 0.062 0.029 0.005 0.010 0.004 0.002 0.003 0.001 0.002	0.401 0.399 0.201 2.019 0.063 0.127 0.301 0.016 0.084 0.042 0.008 0.019 0.007 0.004 0.007 0.004 0.002
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0+4: 0+2: 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	S D P 1-2F 1-3F 1-4F 1-5 1-6 1-7 1-8 R 2 R 8 R 8 R 8 R 9 R 10	Dir 0.161 0.178 0.091 0.000 0.000 0.000 0.050 0.004 0.021 0.002 0.002 0.002 0.004 0.002 0.001 0.001 0.001 0.001 0.000 0.000	Sec 0.240 0.220 0.109 2.019 0.063 0.127 0.251 0.012 0.062 0.029 0.005 0.010 0.004 0.002 0.006 0.003 0.001 0.002 0.009 0.004 0.002	0.401 0.399 0.201 2.019 0.063 0.127 0.301 0.016 0.084 0.042 0.008 0.019 0.007 0.004 0.007 0.004 0.002 0.002 0.009 0.004
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500 KeV

-	cies	Dir	Sec	Total
0+4		0.142	0.259	0.401
0+21	D	0.157	0.242	0.398
0+2	P	0.081	0.120	0.201
0	1-2F	0.000	2.022	2.022
0	1-3F	0.000	0.063	0.063
0	1-4F	0.000	0.127	0.127
0	1-4	0.044	0.257	0.301
0	1-5	0.003	0.013	0.018
0	1-6	0.019	0.065	0.084
0	1-7	0.011	0.031	0.042
o	1-8	0.002	0.005	0.008
o	R 1	0.011	0.011	0.022
o	R 2	0.004	0.004	0.009
0	R 3	0.003	0.002	0.005
ŏ	R 4	0.002	0.008	0.008
ŏ	R 5	0.001	0.003	0.004
0	R 6	0.001	0.001	0.002
Ö	R 7	0.000	0.002	0.002
0	R 8	0.000	0.002	0.009
Ö	R 9	0.000	0.004	0.004
Ö	R10	0.000	0.002	0.002
0	R11	0.000	0.008	0.006
ō	R12	0.000	0.004	0.004
ō	R13	0.000	0.001	0.001
	,			
	77	1 Me	V	
	cies	Dir	Sec	Total
0+4	S·	Dir 0.135	Sec 0.266	0.401
0+4	S ·	Dir 0.135 0.149	Sec 0.266 0.249	0.401
0+4 0+2 0+2	S · D P	Dir 0.135 0.149 0.077	Sec 0.266 0.249 0.124	0.401 0.398 0.201
0+4 0+2 0+2	S D P 1-2F	Dir 0.135 0.149 0.077 0.000	Sec 0.286 0.249 0.124 2.019	0.401 0.398 0.201 2.019
0+4 0+2 0+2 0	S · D · P · 1-2F · 1-3F	Dir 0.135 0.149 0.077 0.000 0.000	Sec 0.266 0.249 0.124 2.019 0.063	0.401 0.398 0.201 2.019 0.063
0+4 0+2 0+2 0 0	S - D - D - D - D - D - D - D - D - D -	Dir 0.135 0.149 0.077 0.000 0.000	Sec 0.266 0.249 0.124 2.019 0.063 0.127	0.401 0.398 0.201 2.019 0.063 0.127
0+4 0+2 0+2 0 0 0	S - D - D - D - D - D - D - D - D - D -	Dir 0.135 0.149 0.077 0.000 0.000 0.000	Sec 0.266 0.249 0.124 2.019 0.063 0.127 0.260	0.401 0.398 0.201 2.019 0.063 0.127 0.301
0+4 0+2 0+2 0 0 0	S - D - D - D - D - D - D - D - D - D -	Dir 0.135 0.149 0.077 0.000 0.000 0.000 0.041 0.003	Sec 0.266 0.249 0.124 2.019 0.063 0.127 0.260 0.013	0.401 0.398 0.201 2.019 0.063 0.127 0.301 0.018
0+4 0+2 0+2 0 0 0 0	S - D - 2F - 1-3F - 1-4F - 1-5 - 1-6	Dir 0.135 0.149 0.077 0.000 0.000 0.000 0.041 0.003 0.018	Sec 0.266 0.249 0.124 2.019 0.063 0.127 0.260 0.013 0.066	0.401 0.398 0.201 2.019 0.063 0.127 0.301 0.016 0.084
0+4 0+2 0+2 0 0 0 0	S - D - 2F - 1-3F - 1-4F - 1-5 - 1-6 - 1-7	Dir 0.135 0.149 0.077 0.000 0.000 0.000 0.041 0.003 0.018	Sec 0.266 0.249 0.124 2.019 0.063 0.127 0.260 0.013 0.066 0.032	0.401 0.398 0.201 2.019 0.063 0.127 0.301 0.016 0.084 0.042
0+4 0+2 0+2 0 0 0 0 0 0	S - D - 2F - 1 - 3F - 1 - 4F - 1 - 5 - 1 - 6 - 7 - 1 - 8	Dir 0.135 0.149 0.077 0.000 0.000 0.000 0.041 0.003 0.018 0.010	Sec 0.266 0.249 0.124 2.019 0.063 0.127 0.260 0.013 0.066 0.032 0.006	0.401 0.398 0.201 2.019 0.063 0.127 0.301 0.018 0.084 0.042 0.008
0+4 0+2 0+2 0 0 0 0 0 0 0	S - D - 2F - 2F - 1 - 3F - 1 - 4F - 1 - 5 - 1 - 6 - 1 - 7 - 1 - 8 R 1	Dir 0.135 0.149 0.077 0.000 0.000 0.041 0.003 0.018 0.010 0.002 0.012	Sec 0.266 0.249 0.124 2.019 0.063 0.127 0.260 0.013 0.066 0.032 0.006 0.011	0.401 0.398 0.201 2.019 0.063 0.127 0.301 0.016 0.084 0.042 0.008 0.023
0+4 0+2 0+2 0 0 0 0 0 0 0	S - 2F 1-2F 1-3F 1-4F 1-4 1-5 1-6 1-7 1-8 R 1	Dir 0.135 0.149 0.077 0.000 0.000 0.041 0.003 0.018 0.010 0.002 0.012	Sec 0.266 0.249 0.124 2.019 0.063 0.127 0.260 0.013 0.066 0.032 0.006 0.011 0.004	0.401 0.398 0.201 2.019 0.063 0.127 0.301 0.016 0.084 0.042 0.008 0.023 0.009
0+42 0+2 0 0 0 0 0 0 0 0	S - D - 2F 1 - 2F 1 - 4F 1 - 4 1 - 5 1 - 6 1 - 7 1 - 8 R 2 R 3	Dir 0.135 0.149 0.077 0.000 0.000 0.041 0.003 0.018 0.010 0.002 0.012 0.005 0.005	Sec 0.266 0.249 0.124 2.019 0.063 0.127 0.260 0.013 0.066 0.032 0.006 0.011 0.004 0.002	0.401 0.398 0.201 2.019 0.063 0.127 0.301 0.016 0.084 0.042 0.008 0.023 0.009 0.005
0+42 0+2 0 0 0 0 0 0 0 0 0 0	S - 2F 1-2F 1-3F 1-4F 1-5 1-6 1-7 1-8 R 1 R 2 R 3	Dir 0.135 0.149 0.077 0.000 0.000 0.041 0.003 0.018 0.010 0.002 0.012 0.005 0.003	Sec 0.266 0.249 0.124 2.019 0.063 0.127 0.260 0.013 0.066 0.032 0.006 0.011 0.004 0.002 0.006	0.401 0.398 0.201 2.019 0.063 0.127 0.301 0.016 0.084 0.042 0.008 0.023 0.009 0.005 0.008
0+42 0+2 0 0 0 0 0 0 0 0 0 0 0 0	S - 2F 1-2F 1-3F 1-4F 1-4 1-5 1-6 1-7 1-8 R 2 R 3 R 5	Dir 0.135 0.149 0.077 0.000 0.000 0.001 0.003 0.018 0.010 0.002 0.012 0.005 0.003 0.003	Sec 0.266 0.249 0.124 2.019 0.063 0.127 0.260 0.013 0.066 0.032 0.006 0.011 0.004 0.002 0.006 0.003	0.401 0.398 0.201 2.019 0.063 0.127 0.301 0.016 0.084 0.042 0.008 0.023 0.009 0.005 0.008
0+42 0+2 0+2 0 0 0 0 0 0 0 0 0 0 0 0	S - 2F 1-3F 1-4F 1-4 1-5 1-6 1-7 1-8 R 2 R 3 R 5 R 6	Dir 0.135 0.149 0.077 0.000 0.000 0.000 0.041 0.003 0.018 0.010 0.002 0.012 0.005 0.003 0.003	Sec 0.266 0.249 0.124 2.019 0.063 0.127 0.260 0.013 0.066 0.032 0.006 0.011 0.004 0.002 0.006 0.003	0.401 0.398 0.201 2.019 0.063 0.127 0.301 0.018 0.084 0.042 0.008 0.023 0.009 0.005 0.005
0+42 0+2 0+2 00 00 00 00 00 00 00 00	SDP 1-3F 1-4F 1-4F 1-5 1-6 1-7 1-8 R R R R R R R R R R R R R R R R R R R	Dir 0.135 0.149 0.077 0.000 0.000 0.000 0.041 0.003 0.018 0.010 0.002 0.012 0.005 0.003 0.003 0.002	Sec 0.266 0.249 0.124 2.019 0.063 0.127 0.260 0.013 0.066 0.032 0.006 0.011 0.004 0.002 0.003 0.003 0.003	0.401 0.398 0.201 2.019 0.063 0.127 0.301 0.016 0.084 0.042 0.008 0.023 0.009 0.005 0.005 0.005
0+420+200000000000000000000000000000000	SDP 1-3F 1-4F 1-4 1-5 1-6 1-7 1-8 R R R R R R R R R R R R R R R R R R R	Dir 0.135 0.149 0.077 0.000 0.000 0.000 0.018 0.010 0.002 0.012 0.005 0.003 0.003 0.003	Sec 0.266 0.249 0.124 2.019 0.063 0.127 0.260 0.013 0.066 0.032 0.006 0.011 0.004 0.002 0.003 0.003 0.002 0.002 0.002	0.401 0.398 0.201 2.019 0.063 0.127 0.301 0.016 0.084 0.042 0.008 0.023 0.009 0.005 0.005 0.005
0+4200000000000000000000000000000000000	SDP 1-4F 1-4 1-5 1-6 1-7 1-8 1 2 3 4 5 6 7 8 9	Dir 0.135 0.149 0.077 0.000 0.000 0.000 0.041 0.003 0.018 0.010 0.002 0.012 0.005 0.003 0.003 0.003 0.003 0.002	Sec 0.266 0.249 0.124 2.019 0.063 0.127 0.260 0.013 0.066 0.032 0.006 0.011 0.004 0.002 0.002 0.005 0.002 0.002 0.002 0.002 0.002	0.401 0.398 0.201 2.019 0.063 0.127 0.301 0.016 0.084 0.042 0.008 0.023 0.009 0.005 0.005 0.005 0.002 0.002
0+4200000000000000000000000000000000000	SDP 1-3F 1-4F 1-4F 1-5 1-6 1-7 1-8 R R R R R R R R R R R R R R R R R R R	Dir 0.135 0.149 0.077 0.000 0.000 0.001 0.003 0.018 0.010 0.002 0.012 0.005 0.003 0.003 0.003 0.003 0.003 0.003 0.000	Sec 0.266 0.249 0.124 2.019 0.063 0.127 0.260 0.013 0.066 0.032 0.006 0.011 0.004 0.002 0.002 0.008 0.003 0.002 0.002 0.002 0.002	0.401 0.398 0.201 2.019 0.063 0.127 0.301 0.016 0.084 0.042 0.008 0.023 0.009 0.005 0.005 0.005 0.002 0.002
0+420+200000000000000000000000000000000	SDP 1-3F 1-4F 1-4F 1-5 1-7 1-8 R R R R R R R R R R R R R R R R R R R	Dir 0.135 0.149 0.077 0.000 0.000 0.001 0.003 0.018 0.010 0.002 0.012 0.005 0.005 0.003 0.003 0.003 0.003 0.000 0.000 0.000	Sec 0.266 0.249 0.124 2.019 0.063 0.127 0.260 0.013 0.066 0.032 0.006 0.011 0.004 0.002 0.008 0.003 0.002 0.002 0.002 0.002 0.002 0.002 0.002 0.002	0.401 0.398 0.201 2.019 0.063 0.127 0.301 0.016 0.084 0.042 0.008 0.023 0.009 0.005 0.005 0.005 0.002 0.002 0.002
0+4200000000000000000000000000000000000	SDP 1-3F 1-4F 1-4F 1-5 1-6 1-7 1-8 R R R R R R R R R R R R R R R R R R R	Dir 0.135 0.149 0.077 0.000 0.000 0.001 0.003 0.018 0.010 0.002 0.012 0.005 0.003 0.003 0.003 0.003 0.003 0.003 0.000	Sec 0.266 0.249 0.124 2.019 0.063 0.127 0.260 0.013 0.066 0.032 0.006 0.011 0.004 0.002 0.002 0.008 0.003 0.002 0.002 0.002 0.002	0.401 0.398 0.201 2.019 0.063 0.127 0.301 0.016 0.084 0.042 0.008 0.023 0.009 0.005 0.005 0.005 0.002 0.002

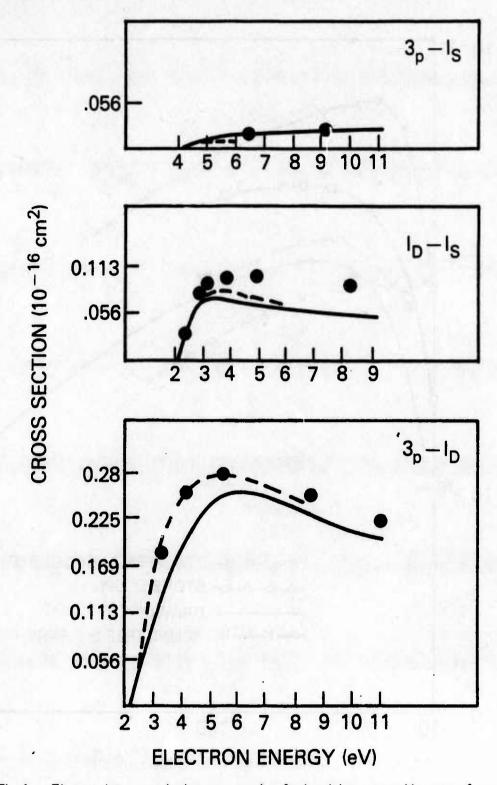


Fig. 1 — Electron impact excitation cross section for low lying metastable states of oxygen, solid curve (Ref. 23) and dashed lines (Ref. 35).

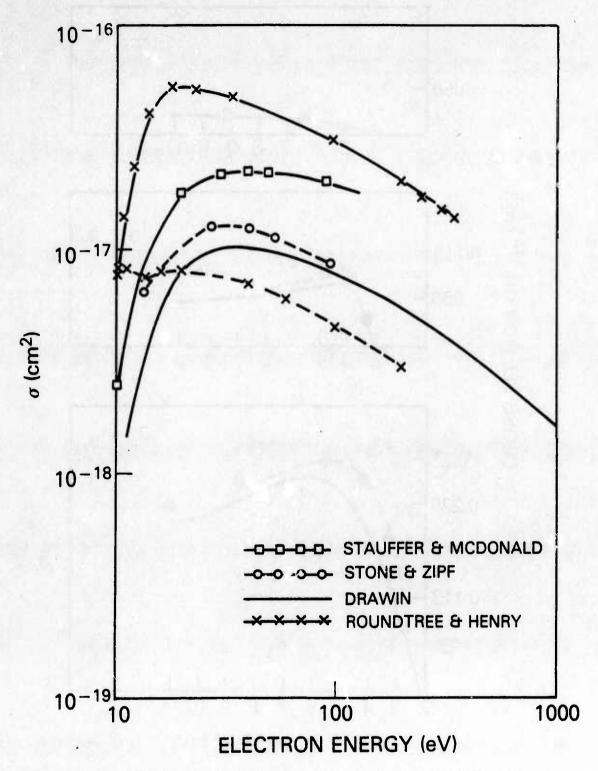


Fig. 2 — Electron impact excitation of the oxygen resonance line. $(3_P - 3_S)$

CROSS SECTIONS

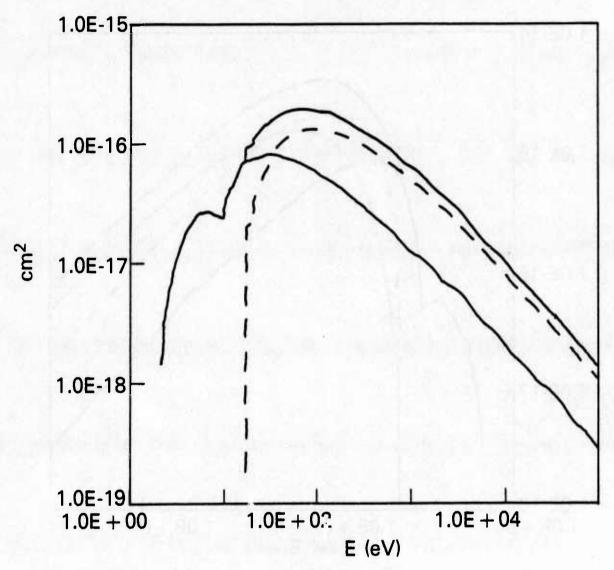


Fig. 3 — Total cross sections in atomic oxygen. The lower solid line is for electronic excitation.

The dashed is for ionization.



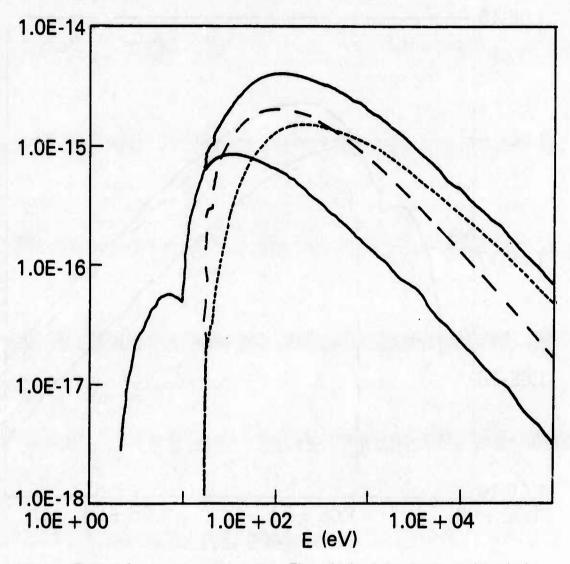


Fig. 4 — The loss function in atomic oxygen. The solid line is loss to electronic excitations. The dashed line is loss to ionization. The dotted line is to secondary electrons.

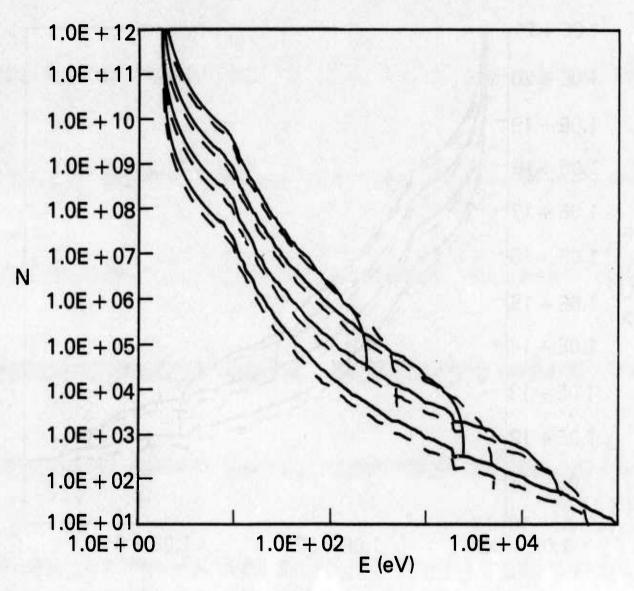


Fig. 5 — Steady state secondary electron distribution function for beam electrons with energies of 500 to 1 MeV.

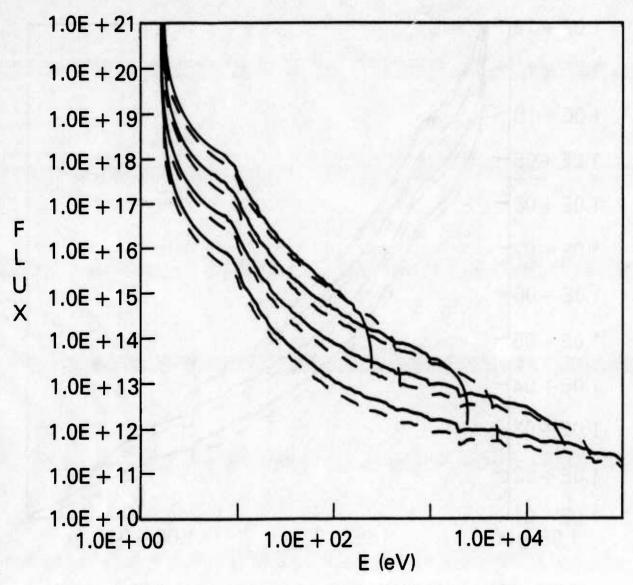


Fig. 6 - Steady state secondary electron flux for beam electron energies of 500 to 1 MeV.

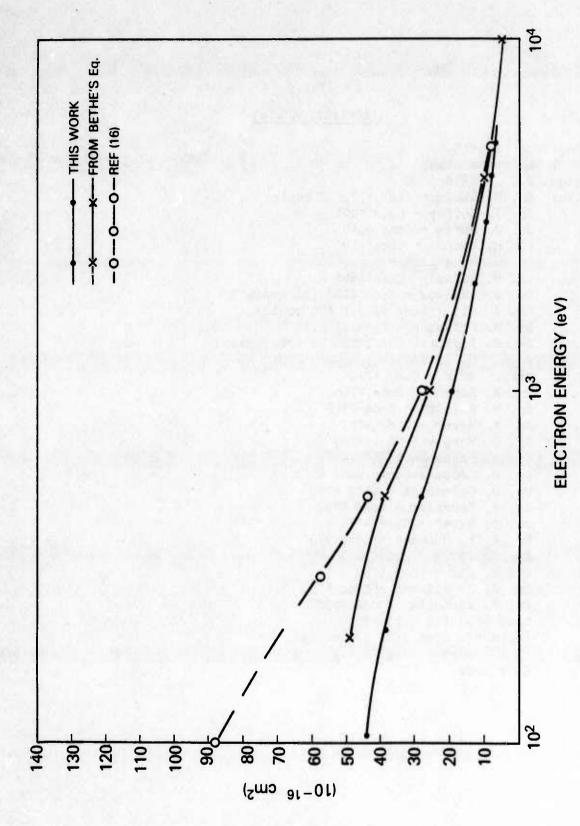


Fig. 7 - Loss function in atomic oxygen. (a comparison)

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